

The Greenhouse Gas Footprint of Liquefied Natural Gas (LNG) Exported from the United States

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Abstract

Liquefied natural gas (LNG) exports from the US have risen dramatically since the LNG-export ban was lifted in 2016, and the US is now the world's largest exporter. This LNG is produced largely from shale gas. Production of shale gas as well as liquefaction to make LNG and LNG transport by tanker are energy-intensive, which contributes significantly to the LNG greenhouse gas footprint. The production and transport of shale gas emit a substantial amount of methane as well, and liquefaction and tanker transport of LNG can further increase methane emissions. Consequently, carbon dioxide (CO₂) from end-use combustion of LNG contributes only 34% of the total LNG greenhouse gas footprint, when CO₂ and methane are compared over 20 years following emission (GWP₂₀). Upstream and midstream methane emissions are the largest contributors to the LNG footprint (38% of total LNG emissions, based on GWP₂₀). Adding CO₂ emissions from the energy used to produce LNG, total upstream and midstream emissions make up on average 47% of the total greenhouse gas footprint of LNG. Other significant emissions are the liquefaction process (8.8% of total, on average, using GWP₂₀) and tanker transport (5.5% of total, on average, using GWP₂₀). Emissions from tankers vary from 3.9% to 8.1% depending upon the type of tanker. Surprisingly, the most modern tankers propelled by 2-stroke and 4-stroke engines have higher total greenhouse gas emissions than steam-powered tankers, despite their greater fuel efficiency and lower CO₂ emissions, due to methane slippage in their exhaust. Overall, the greenhouse gas footprint for LNG as a fuel source is 33% greater than for coal when analyzed using GWP₂₀, (160 g CO₂-equivalent/MJ vs 120 g CO₂-equivalent/MJ). Even considered on the time frame of 100 years after emission (GWP₁₀₀), which severely understates the climatic damage of methane, the LNG footprint equals or exceeds that of coal.

Introduction

In this paper, I analyze the greenhouse gas footprint of liquefied natural gas (LNG) produced in and exported from the United States. The United States prohibited the export of LNG before 2016, but since the lifting of the ban at that time, exports have risen rapidly (DiSavino 2017). In 2022 the United States became the largest exporter of LNG globally (EIA 2023-a). Exports of LNG doubled between 2019 and 2023, and if allowed by the United States government to continue, were predicted to double again over the next four years (Joselow and Puko 2023). As of 2023, the LNG exported from the United States represented 21% of all global LNG transport (IGU 2024). In January of 2024, U.S. President Biden placed a moratorium on increasing exports of LNG pending further study of the consequences of such exports, including the analysis of greenhouse gas emissions (Carbon Brief 2024). An earlier version of the analysis I present in this paper was used by the White House as evidence for the need for greater study on the greenhouse gas emissions from LNG, particularly methane emissions (Clarke 2024).

Proponents of increased exports of LNG from the United States to both Europe and Asia have often claimed a climate benefit, arguing that the alternative would be greater use of coal produced domestically in those regions (Sneath 2023; Joselow and Puko 2023), with increased emissions of carbon dioxide. In fact, even though carbon dioxide emissions are greater from burning coal than from burning natural gas, methane emissions can more than offset this difference (Howarth et al. 2011; Howarth 2014; Howarth and Jacobson 2021; Gordon et al. 2023). As a greenhouse gas, methane is more than 80 times more powerful than carbon dioxide when considered over a 20 year period (IPCC 2021), and so even small methane emissions can have a large climate impact. Clearly, greenhouse gas emissions from LNG must be larger than from the natural gas from which it is made, because of the energy needed to liquefy the gas, transport the LNG, and re-gasify it. The liquefaction process alone is highly energy intensive (Hwang et al. 2014; Pace Global 2015). A lifecycle assessment is required to determine the full magnitude of these LNG greenhouse gas emissions. My analysis builds on earlier lifecycle assessments for LNG (Tamura et al. 2001; Okamura et al. 2007; Abrahams et al. 2015; NETL 2019; Gan et al. 2020; Nie et al. 2020; Rosselot et al. 2021). Of these, only those since 2015 have analyzed LNG export from the United States, and their focus was on export to China. My focus here is on exports from the United States to Europe as well as to China, using the most recent data on methane emissions from shale gas development in the United States.

Most natural gas production in the United States is shale gas extracted using high volume hydraulic fracturing and high-precision directional drilling, two technologies that only began to be used commercially to develop shale gas in this century (Howarth 2019, 2022-a). It is the rapid increase in shale gas production in the United States that has allowed and driven the increase in export of LNG (Joselow and Puko 2023). As shown in Figure 1, production of natural gas in the United States was relatively flat from 1985 to 2005. Since then, production has risen rapidly, driven almost entirely by the production of shale gas. The United States was a net importer of natural gas from 1985 to 2015, with net exports as LNG only since 2016 driven by production in excess of domestic consumption. Shale gas production is quite energetically intensive, and the related emissions of carbon dioxide need to be considered in any full lifecycle assessment of the greenhouse gas emissions associated with LNG. Further, methane emissions from shale gas can be substantial. Since 2008, methane emissions from

shale gas in the United States may have contributed one third of the total (and large) increase in atmospheric methane globally (Howarth 2019, 2022-a).

The types of ships used to transport LNG have been changing in recent years (Huan et al. 2018; Bakkali and Ziomas 2019; Pavlenko et al. 2020), and more than 85% of the global fleet is composed of tankers less than 20 years old (IGU 2024). As of the beginning of 2024, this fleet consisted of 701 tankers, only 21 of them older than 30 years, and 359 new tankers were under construction (IGU 2024). Several different modes of propulsion are common in LNG tankers, including steam power and 4-stroke and 2-stroke engines. The vast majority of these tankers can be powered either burning “boil off” or other fuels, such as diesel or heavy fuel oil. Boil off is the evaporative loss of methane due to some heat leakage through insulation and into the tanks that hold LNG. The only common tankers that cannot use boil off methane for their fuel are slow-speed diesel vessels that instead capture and reliquefy their boil off. These make up approximately 7% of the global fleet, although no new ones have been delivered since 2015, in part because of difficulty in meeting new emission standards (IGU 2024). Steam-powered vessels compose 31.5% of the global fleet. They are relatively inefficient, and so are considered a “superseded technology” (IGU 2024). Another 28% of the fleet is made up of tankers powered by electric motors with electricity provided from 4-stroke generators that can burn two or more fuels (IGU 2024). These are more efficient than steam-powered vessels but have high maintenance costs. Among the newest propulsion technologies is the use of 2-stroke engines powered by either boil off or diesel fuel (IGU 2024). Dual-fuel 2-stroke tankers have greater fuel efficiencies and so are likely to become more common in the future (Huan et al. 2018; Pavlenko et al. 2020).

Emissions of both carbon dioxide and methane vary significantly across these different types of tankers (Rosselot et al. 2023). Tankers powered by 4-stroke and 2-stroke engines are more efficient than are steam-powered tankers, and so have lower carbon dioxide emissions (Bakkali and Ziomas 2019; Pavlenko et al. 2020). However, when these 4-stroke and 2-stroke vessels burn boil off, some unburned methane slips through and is emitted in the exhaust gases (Pavlenko et al. 2020; Balcombe et al. 2021). Steam-powered tankers emit virtually no methane in their exhaust gases which may partially offset their higher emissions of carbon dioxide. These differences in emissions from tankers are a major focus of this analysis, which considers four different types of tankers: 1) steam-powered vessels; 2) tankers that are powered by 4-cycle engines; 3) more modern tankers powered by 2-cycle engines; and 4) tankers that are unable to burn the boil off of LNG and are powered primarily by diesel oil. My analysis relies heavily on three recent, comprehensive assessments of the use of LNG as a marine fuel (Pavlenko et al. 2020; Balcombe et al. 2021; Rosselot et al. 2023).

I present a detailed lifecycle assessment for the LNG system, that estimates emissions from the production of shale gas feedstock through combustion by the final consumer. My analysis focuses on carbon dioxide and methane and excludes other greenhouse gases such as nitrous oxide that are very minor contributors to total emissions for natural gas and LNG systems (Howarth 2020; Pavlenko et al. 2020). Included are emissions of carbon dioxide and methane at each step along the supply chain, including those associated with the production, processing, storage, and transport of the shale gas that is the feedstock for LNG (referred to as upstream and midstream emissions), emissions from the energy used to power the liquefaction of shale gas to LNG, emissions from the energy consumed in transporting the LNG by tanker, emissions from the energy used to re-gasify LNG to gas, and emissions from the

delivery of gas to and combustion by the final consumer. For upstream and midstream methane emissions, I rely on a very recent and comprehensive analysis that used almost one million measurements in the United States (Sherwin et al. 2024). As with some other prior lifecycle assessments for LNG, I explicitly compare the emissions from LNG to those for coal (Abrahams et al. 2015; NETL 2019; Nie et al. 2020; Rosselot et al. 2021). Additionally, I compare the greenhouse gas footprint of LNG with the those of oil and natural gas used domestically and with that for electric-driven heat pumps.

Methods

Calculations use net calorific values (also called lower heating values). Note that the use of net calorific values is standard in most countries, but the United States uses gross calorific values. Emissions expressed using net calorific values are approximately 10% greater than when using gross calorific values (Hayhoe et al. 2002; Howarth et al. 2011; Howarth 2020). LNG and heavy fuel oils are assumed to have energy densities of 48.6 MJ/kg and 39 MJ/kg respectively (Engineering Toolbox 2023). I convert methane emissions to carbon dioxide equivalents using a 20-year Global Warming Potential (GWP₂₀) of 82.5 and a 100-year GWP₁₀₀ of 29.8 (IPCC 2021). Specifying the time frame for comparison is necessary because methane has a far shorter residence time in the atmosphere. The use of GWP₁₀₀ is more common than GWP₂₀, although evidence shows GWP₁₀₀ underestimates the climatic impact of methane, and GWP₂₀ is increasingly being favored in many lifecycle assessments (Howarth 2014, 2020; Ocko et al. 2017; Fesenfeld et al. 2018; Pavlenko et al. 2020; Howarth and Jacobson 2021; Balcombe et al. 2021, 2022; Rosselot et al. 2021). For ease of calculation, this analysis assumes that shale gas and LNG are composed just of methane, ignoring other gases. Table 1 briefly summarizes some of the input parameters for the lifecycle assessment that are detailed below.

Upstream plus midstream emissions:

Upstream plus midstream emissions of both carbon dioxide and methane are based on the total quantity of natural gas and other fuels consumed in the LNG system. In addition to the natural gas burned by the final consumer, natural gas and LNG are burned to provide the energy required for the liquefaction, tanker transport, and regasification processes. The upstream and midstream emissions include emissions in the gas development fields as well as from storage and processing plants and from the high-pressure pipelines that bring natural gas to LNG liquefaction facilities. The following two equations give the upstream plus midstream emissions for methane and carbon dioxide respectively in units of g of methane and g of carbon dioxide per kg of LNG burned by the final consumer:

$$\text{Equation 1} \quad \text{CH}_4 = [(0.028) * (1.028) * (1,000 \text{ g CH}_4/\text{kg}) * \text{LNG.tot}] + [\text{Fuel.oil} * (3.9 \text{ g CO}_4/\text{kg oil})]$$

$$\text{Equation 2} \quad \text{CO}_2 = [(612 \text{ g CO}_2/\text{kg LNG}) * \text{LNG.tot}] + [\text{Fuel.oil} * (616 \text{ g CO}_2/\text{kg oil})]$$

where **LNG.tot** is the total mass of methane gas consumed or emitted, including not only from the final combustion of the regasified LNG fuel but also upstream and midstream, during liquefaction to produce LNG, during transport of LNG in tankers, and emitted from pipelines transporting gas from the LNG

destination port to the final consumer. **Fuel.oil** is the quantity of heavy fuel oil or diesel consumed by ships (for those ships that use these as their primary source of energy) divided by the total quantity of LNG delivered per voyage, in units of kg oil/kg LNG. The calculations for **LNG.tot** and for **Fuel.oil** are shown below in equations #3 and #11.

The methane emission factor for natural gas of 0.028 (2.8% of gas production) used in equation #1 is based on a very recent and comprehensive analysis for upstream and midstream emissions in the United States that combines a very large data set of observations taken by aircraft flyovers with empirically derived simulations (Sherwin et al. 2024). Here, we use their estimates for the Permian Basin, and weigh the upstream emissions by the portion of energy produced as natural gas compared to oil, as recommended by Sherwin et al. (2024). Details are provided in Supplemental Table A and supporting on-line only text. The vast majority of LNG exports from the United States are from Texas and Louisiana (EIA 2023-a). The Permian Basin (west Texas and southeastern New Mexico) and similar oil-associated gas fields are providing most of the gas used for these LNG exports, a trend that is predicted to continue because of proximity of these fields to the LNG export terminals (EIA 2022-a, 2022-b, 2023-b). Methane emissions from producing fuel oil are estimated as 0.10 g CH₄/MJ (NETL 2008; Howarth et al. 2011). With an energy density of 39 MJ/kg, this is equivalent to 3.9 g CH₄/kg fuel oil (Equation #1). The emission factors for indirect carbon dioxide emissions in equation #2 are 612 g CO₂/kg LNG for natural gas and 616 g CO₂/kg for fuel oil (DEC 2021, table A.1, converted to net calorific and metric units, and expressed per mass of fuel using the energy densities provided above). These indirect carbon dioxide emissions are from the energy used to explore and drill gas and oil wells, hydraulically fracture the wells, and process, store, and transport the fuels.

The total mass of methane burned to make carbon dioxide or emitted as methane over the entire life cycle for LNG is calculated in equation #3:

$$\text{Equation 3} \quad \mathbf{LNG.tot} = (1 \text{ kg/kg LNG}) + \mathbf{LNG.liq} + \mathbf{LNG.ship} + \mathbf{Vent.boil.off} + (0.0032 \text{ kg/kg LNG})$$

where 1 kg/kg LNG is the quantity of LNG burned by the final consumer. **LNG.liq** is the total mass of LNG consumed or emitted during the liquefaction process, **LNG.ship** is the mass of LNG consumed by a tanker as fuel (for those tankers that burn LNG) divided by the mass of LNG delivered, in units of g CH₄/kg LNG delivered to the destination port. **Vent.boil.off** is the mass of LNG emitted as methane to the atmosphere by tankers that reliquefy boiled-off methane (due to imperfect capture of this methane) divided by the mass of LNG delivered to the destination port, in units of g CH₄/kg LNG. The value of 0.0032 kg/kg LNG is the gas emitted during pipeline transportation from the LNG terminal to the electric plant where the gas is finally consumed. As is discussed below, my analysis is for the case where LNG is used to produce electricity in the destination country, and the value of 0.0032 kg/kg LNG is for high-pressure delivery pipes from the LNG terminal to an electric plant (Alvarez et al. 2018). Emissions in the destination country would be substantially higher for the case of delivery of gas to homes and commercial buildings for heating (Howarth 2022-b).

The calculation for **LNG.ship** is shown below in equation #8. The calculation for **Vent.boil.off** is described below in equation #10. **LNG.liq** is calculated by summing the mass of gas burned to produce the CO₂ emissions for liquefaction shown in equation #4 below (converted from mass of CO₂ to mass of CH₄ by dividing by 44 g/mol and multiplying by 16 g/mol) and the mass of methane emitted during liquefaction shown in equation #5 below (converted to units of kg/kg LNG).

Emissions at liquefaction plants:

A substantial amount of energy is required to liquefy methane into LNG, and this energy is provided by burning natural gas. That is, natural gas is both the feed source and energy source used to produce LNG (Hwang et al. 2014). Equations #4 and #5 show the emissions of methane and carbon dioxide from the liquefaction process, in units of g CH₄/kg LNG burned by the final consumer and g CO₂/kg LNG burned by the final consumer. Note that emissions of both methane and carbon dioxide from the liquefaction process are larger when expressed per kg of final consumption than per kg of LNG liquefied.

$$\text{Equation 4} \quad \text{CH}_4 = (3.5 \text{ g CH}_4/\text{kg LNG}) * (1 \text{ kg/kg LNG} + \text{LNG.ship} + \text{Vent.boil.off} + 0.0032 \text{ kg/kg LNG})$$

$$\text{Equation 5} \quad \text{CO}_2 = (270+57+18 \text{ g CO}_2/\text{kg LNG}) * (1 \text{ kg/kg LNG} + \text{LNG.ship} + \text{Vent.boil.off} + 0.0032 \text{ kg/kg LNG})$$

These two equations are simply multiplying emission factors applicable to the liquefaction process by the total amount of LNG that is transported away from the liquefaction plant in tankers, including LNG burned by the final consumer, LNG burned or emitted by tankers, and methane emissions from pipelines in the destination country that carry gas to the final consumer. As noted for equation #3 above, the value of 1 kg/kg LNG represents the LNG burned by the final consumer, and the value of 0.0032 kg/kg LNG is the methane emitted during pipeline transportation from the LNG terminal to the electric plant where the gas is finally consumed (Alvarez et al. 2018).

In equation #4, 3.5 g CH₄/kg LNG is the total rate of release of unburned methane during liquefaction and for regasification based on the mean from the review by Balcombe et al. (2021). Note that a recent paper (Innocenti et al. 2023) reported a lower value, which may represent a best case of what is possible, since they required the cooperation from owners of the LNG facilities (Frank 2023). The higher value from Balcombe et al. (2021) seems likely to be more representative of standard industry performance. For equation #5, the values 270 g CO₂/kg LNG, 57 g CO₂/kg LNG, and 18 g CO₂/kg LNG are respectively the quantities of carbon dioxide emitted from burning gas to power liquefaction, from the CO₂ that was in the natural gas before processing, and from carbon dioxide produced from flaring. Carbon dioxide emissions from the combustion of the gas powering the plants have been measured at many facilities in Australia, Alaska, Brunei, Malaysia, Indonesia, Oman, and Qatar, with emissions varying from 230 to 410 g CO₂/kg of LNG liquefied (Tamura et al. 2001; Okamura et al. 2007). Here, I use the mean estimate of 270 g CO₂/kg LNG liquefied, which is equivalent to 9.8% of the natural gas being liquefied. This is comparable to the value used by Balcombe et al. (2021) in their lifecycle assessment and is at the very low end of emission estimates provided by Pace Global (2015) for guidance for new plants built in the United States: 260 to 370 g CO₂ per kg of LNG liquefied. My estimate is therefore conservative. In addition, carbon dioxide present in unprocessed natural gas, which sometimes contains significant quantities of carbon dioxide, is emitted to the atmosphere as the methane in natural gas is liquefied. These emissions are estimated as 23 to 90 g CO₂/kg of LNG liquefied (Tamura et al. 2001; Okamura et al. 2007). Here I use a mean estimate of 57 g CO₂/kg. In addition, some natural gas is flared at liquefaction plants to maintain gas pressures for safety, with a range of

measured carbon dioxide emissions from zero up to 50 g CO₂/kg of LNG, and a mean estimate of 18 g CO₂/kg (Tamura et al. 2001; Okamura et al. 2007).

Volume of LNG tanker cargo and length of tanker voyages:

Emissions of both carbon dioxide and methane from LNG tankers depend on the size of the tanker and the length of cruises. Most LNG tankers have total capacities between 125,000 to 150,000 m³ (Bai and Jin 2016). In this analysis, I use a value of 135,000 m³, or 67,500 tons LNG (Raza and Schoyne 2014). Generally, not all of the gross LNG cargo is unloaded at the point of destination. Some is retained for the return voyage, both to serve as fuel and to keep the LNG tanks supercooled. Here, I assume that 90% of the cargo is unloaded (Raza and Schoyen 2014). Therefore, the average delivered cargo is 60,800 tons LNG.

For the length of the voyage, I use the global average distance for LNG tankers (16,200 km each way) as well as the shortest regular commercial route from the US (9,070 km each way, Sabine Pass, TX to the UK;) and the longest regular commercial route from the US (27,961 km each way, Sabine Pass, TX to Shanghai; Oxford Institute for Energy Studies 2018). Most of LNG exports from the US are from the Sabine Pass area, so these distances well characterize US exports (Joselow and Puko 2023). Considering the average speed of 19 knots (35.2 km per hour; Oxford Institute for Energy Studies 2018), these cruise distances correspond to times of 19 days, 10.7 days, and 35 days each way, respectively, or 38 days, 21.4 days, and 70 days roundtrip. Note that the travel distances for LNG tankers have been increasing over time (Timera Energy 2019). In 2023, a drought limited the capacity of the Panama Canal, leading to LNG tankers from Texas to Asia taking longer routes through the Suez Canal or south of Good Hope in Africa (Williams 2023).

Emissions during transport by LNG tankers:

The carbon dioxide emissions during LNG transport are largely from the combustion of the fuel that powers the tankers and related equipment onboard the vessels, such as generators. Methane emissions are largely from the incomplete combustion of fuel by 4-cycle and 2-cycle tankers, with release of unburned methane in the exhaust gases. As noted in the introduction, my analysis considers four different types of tankers: 1) steam-powered vessels; 2) tankers that are powered by 4-cycle engines; 3) modern tankers powered by 2-cycle engines ; and 4) tankers that are unable to burn the boil off of LNG and that are powered by diesel oil. Here, I assume that any tanker that can use LNG for its fuel will meet virtually all of its fuel needs from this source. Although most tankers can burn heavy fuel oil and/or diesel oil, consumption of these fuels tends to be very low compared to LNG (Raza and Schoyen 2014; Bakkali and Ziomas 2019; Balcombe et al. 2022), except in those rare times when LNG prices are high relative to fuel oils (Jaganathan and Khasawneh 2021). And while it might be expected that tankers would burn fuel oil if the rate of unforced boil off were not sufficient, most tankers instead are likely to force more boil off for their fuel, if necessary, in part to meet stringent sulfur emission standards for ships that went into effect in 2020 (Bakkalil and Ziomas 2019).

Emissions of methane and carbon dioxide are calculated using equations #6 and #7, with units of g CH₄/kg LNG burned by the final consumer and g CO₂/kg LNG burned by the final consumer.

Equation 6 $CH_4 = [LNG.ship * Slip * 1,000] + Vent.boil.off$

Equation 7 $CO_2 = [LNG.ship * (44 \text{ g } CO_2/mol)/(16 \text{ g } CH_4/mol) * 1,000 \text{ g } CH_4/kg \text{ } CH_4]$
 $+ [Fuel.oil * (80 \text{ g } CO_2/MJ \text{ oil}) * (39 \text{ MJ/kg oil})]$

where **Slip** is the fraction of the burned LNG fuel that is emitted unburned as methane in the exhaust stream. Equation #7 converts the mass of LNG methane consumed by ships for fuel to the mass of carbon dioxide emitted using. The value of 80 g CO₂/MJ is the carbon dioxide emission factor per unit of energy for fuel oil (Pavlenko et al. 2020) and 39 MJ/kg is the energy density for fuel oil.

For vessels powered by 4-stroke engines, I assume **Slip** is 0.064 (6.4%) of the LNG burned by the tanker, the average value measured by Comer et al. (2024) in a recent campaign using drones, helicopters, and on-board measurements at sea. This is significantly higher than the values assumed by Balcombe et al. (2021) and by Pavlenko et al. (2020). For tankers powered by 2-stroke engines burning LNG, I assume a 0.038 methane slip rate based on data in Balcombe et al. (2022) for a newly commissioned tanker. Note that this is higher than 0.023 reported in Balcombe et al. (2021) or values reported in Pavlenko et al. (2020), due to emissions of unburned methane from electric generators, which are necessary for tankers powered by 2-stroke engines. Methane emissions in the exhaust of steam-powered tankers are negligible, as are emissions from burning diesel (Pavlenko et al. 2020), and are ignored in this analysis.

Equation #8 provides the estimation for LNG consumed by tankers that burn LNG, normalized to the mass of LNG delivered.

Equation 8 $LNG.ship = Days * (LNG.fuel / 60,800,000 \text{ kg LNG})$

where **Days** is the number of days for a round-trip cruise to and from the liquefaction facility, **LNG.fuel** is the rate of LNG consumption per day, and 60,800,000 kg LNG is the average delivered cargo, as discussed above. Fuel consumption rates are assumed to be 175 tons LNG per day for steam-powered tankers, 130 tons LNG per day for ships powered by 4-cycle engines, and 108 tons LNG per day for ships powered by modern 2-cycle engines (Raza and Schoyen 2014; Bakkali and Ziomas 2019).

The unforced boil off of methane during the voyage is calculated in equation #9.

Equation 9 $Boil.off = (0.00135 \text{ kg } CH_4/kg \text{ LNG per day}) * Days * (1,000 \text{ g } CH_4/kg \text{ } CH_4)$

where **Boil.off** is the evaporation from the tankers' LNG tanks during the voyage that occurs from thermal seepage through the insulation of the tanks' insulation. The value 0.00135 kg CH₄/kg LNG per day is the average rate of boil off of methane, equivalent to 0.135% per day of the LNG cargo, normalized to the volume of the cargo. This is the mean value for LNG tankers, with rates as low as 0.1% per day at ambient temperatures of 5° C and as high as 0.17% per day at temperatures of 25° C (Hassan et al. 2009; Huan et al. 2018; BrightHub Engineering 2022; Rosselot et al. 2023). Note that boil off occurs not only during the laden voyage transporting the LNG: some LNG is retained as ballast for the return voyage back to the LNG loading terminal. This is necessary to keep the tanks at low

temperature, and the mass of methane boiled off per day during the return ballast voyage is essentially the same as during the laden voyage (Hassan et al. 2009).

$$\text{Equation 10} \quad \mathbf{Vent.boil.off} = 0.0035 * \mathbf{Boil.off} * \% \mathbf{Reliq}$$

where **%Reliq** is the percentage of **Boil.off** that is not used as fuel by the tanker, but rather is reliquefied. Note that in the past, some tankers simply vented all of the boiled-off methane (Hassan et al. 2009; Bright Hub Engineering 2022). Even today, most tankers are not equipped to reliquefy boil off, but these only vent boil off in excess of their use for fuel. The assumed fraction of methane emitted during reliquefaction, 0.0035, is the same as assumed for shore-based liquefaction plants discussed above.

The quantity of fuel oil or diesel burned by ships, for those ships not burning LNG, is calculated by equation #11.

$$\text{Equation 11} \quad \mathbf{Fuel.oil} = (167,000 \text{ kg oil/day}) * \mathbf{Days} / (60,800,000 \text{ kg LNG})$$

where 167,000 kg oil per day is the rate at which a tanker burns fuel oil and 60,000,800 kg LNG is the quantity of LNG delivered per average cruise. The value of 167,000 kg oil per day is based on data in Bakkali and Ziomas (2019) which indicated an equivalent fuel burn rate of 115 ton LNG/day for slow-speed diesel tankers, assuming 80 g CO₂/MJ for fuel oil and 55 g CO₂/MJ for LNG (Pavlenko et al. 2020).

Final distribution and combustion:

In addition to the methane emissions from upstream and midstream sources before the gas is liquefied to become LNG, considered above, emissions occur after regasification and delivery to the final customer. These emissions are less if the gas is used to generate electricity than if it is delivered to homes and buildings. For the analysis presented in this paper, I only consider the case of electricity generation. For this, methane emissions from transmission pipelines and storage in the destination country are estimated as 0.32% of the final gas consumption (Alvarez et al. 2018), or 0.0032 kg of methane per kg of LNG consumed. As noted above, emissions would be higher for gas used to heat homes and commercial buildings (Howarth 2022-b).

When the gas is burned by the final consumer, I use carbon dioxide emissions of 2,750 g CO₂/kg of LNG delivered. This is based on the stoichiometry of carbon dioxide (44 g/mole) and methane (16 g/mole). It is equivalent to 55 g CO₂/MJ for natural gas (Hayhoe et al. 2002) and is also the value assumed by the IMO 2021) for burning LNG in tankers. Methane is never burned with 100% efficiency, and so there is likely some slippage of unburned methane from the combustion. However, I am aware of no data on this for electric power plants, and assume no slippage in this analysis, to be conservative.

Comparison to natural gas, diesel oil, coal, and heat pumps:

The emission factors for methane and carbon dioxide for natural gas that is used domestically (that is, not converted to LNG) are calculated in equations #12 and #13, in units of g CH₄ or g CO₂ per MJ of energy produced.

$$\text{Equation 12} \quad \text{CH}_4 = (0.0312) * (1.0312) * (55 \text{ g CO}_2/\text{MJ}) * (\text{mol} / 44 \text{ g CO}_2) * (16 \text{ g CH}_4/\text{mol})$$

$$\text{Equation 13} \quad \text{CO}_2 = (55 \text{ g CO}_2/\text{MJ}) + (12.6 \text{ g CO}_2/\text{MJ})$$

where 0.0312 is the fraction of natural gas that is emitted unburned as methane. This includes 0.028 (2.8%) for upstream and midstream emissions (Sherwood et al. 2024) and 0.0032 (0.32%) for downstream emissions (Supplemental Table A), assuming the gas is used for generation of electric power and not for heating of homes and commercial buildings. These are the same values used for the LNG emission calculations. The value of 55 g CO₂/MJ is for the emissions when the gas is burned (EIA 2016, converted to net calorific values), and 12.6 g CO₂/MJ are the indirect emissions from the energy used to develop, process, and transport the gas (DEC 2021, Table A-1, converted to net calorific and metric units).

The emission factors of methane and carbon dioxide for coal that is used domestically (not transported long distances by ship) are shown in equations #14 and #15.

$$\text{Equation 14} \quad \text{CH}_4 = 0.21 \text{ g CH}_4/\text{MJ}$$

$$\text{Equation 15} \quad \text{CO}_2 = (99 \text{ g CO}_2/\text{MJ}) + (3.4 \text{ g CO}_2/\text{MJ})$$

where 0.21 g CH₄/MJ is the emissions factor for methane from the production of coal in the US based on IPCC data (Howarth 2020, converted to net calorific values), 99 g CO₂/MJ are the direct emissions when the coal is burned (EIA 2016, converted to net calorific values), and 3.4 g CO₂/MJ are the indirect emissions from the energy used to develop and transport the coal (DEC 2021, Table A-1, converted to net calorific and metric units). Note that the emission factors used here are significantly larger for methane and somewhat less for indirect carbon dioxide emissions than used by NETL (2019). Note further that the emission factor for methane is very similar to the mean estimate for deep coal mines in China (0.23 g CH₄/MJ; Wang et al. 2019) and for average mining operations in Poland (0.19 g CH₄/MJ; Patynska 2014).

The emission factors of methane and carbon dioxide for diesel oil that is produced domestically are shown in equations #16 and #17.

$$\text{Equation 16} \quad \text{CH}_4 = 0.40 \text{ g CH}_4/\text{MJ}$$

$$\text{Equation 17} \quad \text{CO}_2 = (75 \text{ g CO}_2/\text{MJ}) + (15.8 \text{ g CO}_2/\text{MJ})$$

where 0.40 g CH₄/MJ is the emissions factor for methane from the production of diesel oil, 75 g CO₂/MJ are the direct emissions when the oil is burned (EIA 2016, converted to net calorific values), and 15.8 g CO₂/MJ are the indirect emissions from the energy used to develop and transport diesel oil (DEC 2021, Table A-1, converted to net calorific and metric units). The methane emission factor is from data presented in supplemental materials for Sherwin et al. (2024) and is based on oil production from the

Permian Basin, apportioning upstream methane emissions to the percent of energy produced that is oil compared to natural gas (58%).

Much natural gas is used to heat homes and commercial buildings, not just for electricity. Heat pumps provide an alternative for this heating. To evaluate the greenhouse gas footprint of a heat pump, we use the average emissions from the electric grid in Europe in 2022, reported as 251 g CO₂-eq/kwh, or 70 g CO₂-eq/MJ (European Environment Agency 2023). The average ground-source heat pump has a Coefficient of Performance (COP) of 4.8 (Heat Pumps 2024). The emissions for using a heat pump are estimated by dividing the average grid emissions by the COP.

Results and Discussion

Boil off and LNG consumption by tankers:

The rate of LNG used to power tankers is compared with unforced boil off in Table 2, for those tankers that can burn LNG. The unforced boil off predicted from the assumed percentage of gross cargo per day, 0.1% at an ambient temperature of 5° C and 0.17% at a temperature of 25° C (Hassan et al. 2009), is always less than the fuel required for tankers powered by steam turbines and 4-stroke engines. This is also true for tankers powered by modern 2-stroke engines at the lower temperature. My analysis therefore assumes that these tankers force additional boil off to meet their fuel needs (Bakkali and Ziomas 2019), and this additional forced boil off is included in the overall lifecycle assessment for each type of tanker. For tankers powered by modern 2-stroke engines at the higher temperature, the 115 tons LNG per day as unforced boil off exceed the fuel requirement of 108 tons LNG per day, although not by much (Table 2). These tankers are likely to be equipped with equipment to re-liquefy boil off in excess of their fuel needs. Consequently, I assume that no boil off from these tankers is vented to the atmosphere and that all is captured.

Comparison of emissions of CO₂ from final combustion to methane and indirect CO₂ emissions:

Table 3 presents emissions of carbon dioxide, methane, and total combined emissions expressed as CO₂-equivalents for each of the four scenarios considered, using different types of tankers and the global average time for voyages. Emissions are separated into the upstream plus midstream emissions, those from liquefaction of gas into LNG, emissions from the tankers, emissions associated with the final transmission to consumers, and direct emissions as the gas is burned by the final consumer to produce electricity. These emissions are also summarized in Figure 2 for the shortest and longest voyage times as well as average voyage time, with emissions broken down into the carbon dioxide emitted as the fuel is burned by the final consumer, other carbon dioxide emissions, and emissions of unburned methane. For both Figure 2 and the combined emissions presented in Table 3, methane emissions are compared to carbon dioxide using GWP₂₀ (IPCC 2021). Total emissions are comparable across all four scenarios using different types of tankers, ranging from 7,370 to 8,028 g CO₂-equivalents/kg of LNG consumed for the average round-trip voyage length of 38 days (Table 3). Results using GWP₁₀₀ rather than GWP₂₀ are presented in a later section of this paper. As discussed in the Methods section above, many researchers increasingly favor GWP₂₀ for lifecycle assessments, since this

better capture the effects of methane on the climate system (Ocko et al. 2017; Fesenfeld et al. 2018; Pavlenko et al. 2020; Howarth and Jacobson 2021; Balcombe et al. 2021, 2022; Rosselot et al. 2021).

The direct carbon dioxide emissions from final combustion are important but not a dominant part of total greenhouse gas emissions across all four scenarios. These final-combustion emissions make up 35% to 37% of total greenhouse gas emissions across the four scenarios (Table 3). The largest component of the emissions is from upstream and midstream sources, from producing, processing, storing, and transporting natural gas. The combined emissions for both carbon dioxide and methane from upstream and midstream sources contribute 46% to 48% of total emissions for delivered LNG (Table 3). Indirect carbon dioxide emissions are an important part of these upstream and midstream emissions, reflecting the use of fossil fuels to power the shale gas extraction and processing systems, and make up 9.4% to 9.9% of total emissions across the scenarios (Table 3). Methane emissions from upstream and midstream sources are larger (expressed as carbon-dioxide equivalents), contributing 36% to 38% of total emissions for delivered LNG (Table 3).

The liquefaction process is an important source of emissions of both carbon dioxide and methane, reflecting the large amount of energy needed to super cool methane to liquid form and the release of some unburned methane at liquefaction facilities (Table 3). Total liquefaction emissions are the third largest source of emissions, after the upstream and midstream emissions and emissions of carbon dioxide from the combustion of gas by the final customer, for all four scenarios, ranging from 8.6% to 9% of total emissions (Table 3).

Tanker emissions are the most variable of the emissions across the scenarios considered, ranging from 3.6% of total emissions in the case where LNG is moved by tankers burning diesel oil to 8.1% when LNG is moved by tankers powered with 4-stroke engines when both carbon dioxide and methane are considered (Table 3). The emissions of carbon dioxide by tankers are 2.4% of total emissions for 2-stroke-engine tankers, 2.8% for 4-stroke-engine tankers, 3.9% for steam-powered tankers, and 4.4% for tankers powered by diesel engines (Table 3), reflecting the different fuel efficiencies of these modes of propulsion. However, the two least efficient types of tankers have zero methane slip emissions, while the more efficient tankers powered by 2-stroke and 4-stroke engines emit significant methane, 2.8% and 5.3% respectively of total emissions for delivered LNG (Table 3). These methane emissions, which result from slippage of methane emitted unburned in the exhaust stream (Pavlenko et al. 2020; Balcombe et al. 2021, 2022), more than offset the lower carbon dioxide emissions. Note that my analysis assumes no methane emissions from imperfect capture of boil off used for fuel. I conclude that modern 2-stroke and 4-stroke powered tankers may emit 30% to 215% more total emissions than do steam-powered tankers, despite the lower fuel efficiencies and higher carbon dioxide emissions for steam. Methane slip makes up 53% of the total tanker emissions for tankers powered by 2-stroke engines and 66% for those powered by 4-stroke engines. Similarly, Rosselot et al. (2023) concluded that methane slip made up 54% of total emissions for a very modern tanker powered with a 2-stroke engine

Methane emissions from the final transmission of gas from the regasification terminal to the consumer are relatively small, only 264 g CO₂-equivalents/kg LNG delivered, for all the different tanker scenarios, ranging from 3.3% to 3.4% of total emissions (Table 3). This is because my analysis focuses on

the use of LNG to produce electricity, and the transmission pipelines that deliver gas to such facilities generally have moderately low emissions (Alvarez et al. 2018). However, LNG is also used to feed gas into urban pipeline distribution systems for use to heat homes and commercial buildings. Methane emissions for these downstream distribution systems can be quite high, with the best studies in the United States finding that 1.7% to 3.5% of the gas delivered to customers leaks to the atmosphere unburned (see summary in Howarth 2022-b and references therein). This corresponds to a range of 1,400 to 2,890 g CO₂-equivalents per kg LNG delivered, increasing the total greenhouse gas footprint of LNG by up to 35% above the values shown in Table 3. Emissions from distribution systems are not as well characterized in either Europe or Asia as in the United States (Howarth 2022-b), although one study suggests emissions in Paris, France are in the middle range of those observed in the United States (Defratyka et al. 2021).

Importance of cruise length:

My analysis includes scenarios with the shortest and longest cruise distances from the United States, in addition to the world-average distance shown in Table 3. See Figure 2 and Supplemental Tables B and C for detailed emission estimates from these shortest and longest voyages. The shortest distance represents a voyage from the Gulf of Mexico loading port to the United Kingdom, while the longest distance is for a voyage from the Gulf of Mexico to Shanghai, China, not going through the Panama Canal. Not surprisingly, total emissions go down for the shorter voyage and increase for the longest voyage for all four scenarios considered. This is particularly true for the scenario where boil off from LNG is used to power tanker transport (Figure 2, Supplemental Table B, Supplemental Table C). For all four scenarios, emissions from fuel consumption increase or decrease as travel distances and time at sea increase or decrease. The upstream and downstream emissions and emissions from liquefaction also increase or decrease as the travel distances change, when expressed per mass of LNG delivered to the final consumer. This reflects an increase or decrease in the total amount of LNG burned or boiled off by tankers during their voyages. Qualitatively, the patterns described above based on world average tanker travel distances (Table 3) hold across the cases for shorter and longer voyages. In all cases, total greenhouse gas emissions exceed the direct carbon dioxide emissions when the LNG is burned by the final consumer, by 2.6-fold to 2.8-fold for the shortest cruises (Supplemental Table B) and by 2.8-fold to 3.2-fold for the longest cruises (Supplemental Table C). Upstream and midstream emissions, particularly for methane, are a dominant feature across all time frames and transport by all types of tankers.

Comparison to natural gas, diesel oil, coal, and heat pumps:

Figure 3 compares the greenhouse gas footprint of LNG for the shortest and longest voyage distances to those of coal used domestically near the site of production, natural gas that is not liquefied but rather used domestically, and diesel oil, based on GWP₂₀ for comparing methane to carbon dioxide. Table 4 also shows this comparison with LNG tankers for the average tanker-cruise length, using the average emissions across the three scenarios for transport of LNG by tankers burning LNG boil off for their fuel. The carbon dioxide emissions just from combustion are substantially greater for coal, 99 g CO₂/MJ vs 55 g CO₂/MJ for LNG. Total carbon dioxide emissions from coal, including emissions from developing and transporting the fuel, are also greater than for LNG, but the difference is less, 102.4 g CO₂/MJ for coal vs 83.1 g CO₂/MJ for LNG (Table 4). This is because of greater energy costs and

therefore higher emissions of carbon dioxide for developing and transporting the LNG compared to coal. Methane emissions for LNG are substantially larger than for coal, 76.5 g CO₂-equivalents/MJ for LNG compared to only 17.3 g CO₂-equivalents/MJ for coal (Table 4). As presented above in the Methods section, this result for methane emissions for coal is quite robust across regions, including China and Poland (Wang et al. 2019; Patynska 2014). Consequently, total greenhouse gas emissions are 33% larger for LNG than for coal for the cases of average tanker cruise lengths, 160 g CO₂-equivalent/MJ for LNG vs 120 g CO₂-equivalent/MJ for coal (Table 4).

Natural gas used domestically in the United States (that is not liquefied to LNG) for electricity production has a greenhouse gas footprint that is very similar to that of coal (Figure 3) when methane emissions are included using GWP₂₀, as we have previously demonstrated (Howarth and Jacobson 2021). Neither natural gas nor coal used domestically in the United States has a large climate advantage over the other (Gordon et al. 2023). The greenhouse gas footprint for diesel oil from the Permian Basin is also similar to that of coal (Figure 3; Table 4). However, the footprint for LNG is greater than that of coal, diesel oil, or natural gas even in the case of the shortest cruises. The greenhouse gas footprint for LNG is 28% greater than that of coal for the shortest cruises and 46% greater for the longest cruises (Figure 3).

Also shown in Figure 3 are the greenhouse gas emission estimates for using a ground-source heat pump to heat a home or commercial building, with the pump powered by the average grid electricity for Europe in 2022, as described in the Methods section. Overall emissions are very low, less than 10% of those from burning natural gas, since heat pumps are extremely efficient and gain most of their heat from the environment, not from the electricity. These heat-pump emissions would be zero if the electricity were from 100% renewable sources. Even if the electricity came completely from burning coal, rather than the average European grid energy mix, emissions would be relatively low for the heat pump: 55 g CO₂-eq/MJ, assuming the coal power plant had an efficiency of 45%. Clearly heat pumps are far better than heating with LNG from the standpoint of greenhouse gas emissions.

Comparison with prior studies:

My estimates for the greenhouse gas footprint for LNG exports are at the upper end of those presented in previous studies. Rosselot et al. (2021) provide estimates for LNG exported from the United States to China, based on scenarios where the LNG is produced from a gas field in East Texas with relatively low upstream methane emissions and from a gas field in the Permian basin with higher methane emissions. Using data from their Supplemental Figure S-5, I calculate total emissions of 95 g CO₂-equivalent/MJ for the East Texas LNG and 175 g CO₂-equivalent/MJ for the LNG produced with gas from the Permian, based on GWP₂₀. These values are 40% lower and 9% higher, respectively, than my estimate of 160 g CO₂-equivalent/MJ (Table 4). Note that Rosselot et al. (2021) concluded that LNG produced from gas fields with high methane emissions would be worse than coal from a climate perspective, in agreement with my conclusion. Abrahams et al. (2015) show total pre-combustion emissions (that is, all emissions other than final combustion) as 86 g CO₂-equivalent/MJ when using GWP₂₀ (their Table S-7). Adding in the emissions for final combustion of 55 g CO₂/MJ (Table 4), total emissions are 141 CO₂-equivalent/MJ, or 12% lower than my estimate. Gan et al. (2020) show the non-combustion emissions of exporting LNG to be in the range of 25 to 90 g CO₂-equivalent/MJ (their

Supplemental Fig 1, using GWP₂₀). Given combustion emissions of 55 g CO₂/MJ, total emissions would be 80 to 145 g CO₂-equivalent/MJ, or 9% to 50% less than my estimate. The Gan et al. (2020) estimates are based on the GREET model maintained by the US Department of Energy. The NETL (2019) report also uses the GREET model, and produces similar results: 102 g CO₂-equivalent/MJ for total emissions using GWP₂₀ (calculated from information in Supplemental Table S-4 of Rosselot et al. 2021), a value near the middle of those from Gan et al. (2020) and 36% lower than my estimate.

A key reason that some of these other studies find that total emissions are lower than what I report here is their use of lower estimates for upstream and midstream emissions of methane. Specifically, the studies by Gan et al. (2020) and NETL (2019) use the default methane estimates in the GREET model, which are derived from inventory estimates from the US Environmental Protection Agency. The EPA inventory estimates in turn are based on unverified self-reporting from the oil and gas industry, and are clearly too low compared to data derived from independent sources published in the peer-reviewed literature (Howarth 2022). My study relies on the most robust estimates available for estimates of methane emissions from upstream and midstream sources (Sherwin et al. 2024).

For estimation of total emissions from coal, my estimate of 119.7 g CO₂-equivalent/MJ is well within the range presented in other studies, such as the estimate of 106.6 g CO₂-equivalent/MJ used by NETL (2019) and the estimate of 125 g CO₂-equivalent/MJ from Abrahams et al. (2015), using GWP₂₀.

GWP time frame – sensitivity and significance:

My analysis is sensitive to the global warming potential that is used, as seen in the on-line only Supplemental Figures A and B. Using GWP₁₀₀ of 29.8 instead of GWP₂₀ of 82.5 (IPCC 2021), as was used in Figures 2 and 3, decreases the methane emissions expressed as carbon-dioxide equivalents by a factor of 2.77 (ie, 82.5/29.8). While methane emissions are larger than direct or indirect carbon dioxide emissions when considered through the GWP₂₀ lens for all four scenarios (Figure 2), the direct emissions of carbon dioxide from the final combustion of LNG are larger than methane emissions across all four of the scenarios when using GWP₁₀₀ (Supplemental Figure A). Similarly, the greenhouse gas footprints of LNG and natural gas that is not liquefied decrease relative to coal when viewed through the lens of GWP₁₀₀ (Supplemental Figure B; Figure 3) since methane emissions from coal are less than from natural gas and LNG. Total greenhouse gas emissions from LNG estimated using GWP₁₀₀ are equal to those for coal in the scenario with short voyages but are still greater (by 12%) for the longest cruises (Supplemental Figure B). That is, even using GWP₁₀₀, the greenhouse gas footprint of LNG is always as large as or larger than that of coal. The greenhouse gas footprint of LNG is always substantially worse than that of natural gas used domestically, whether estimated with GWP₂₀ or GWP₁₀₀ (Figure 3, Supplemental Figure B). This must be true, since the LNG is made from natural gas but requires substantial energy to liquefy and transport to market.

Concluding thoughts:

Much of my analysis focuses on comparing the influence of different types of tankers on the LNG greenhouse gas footprint. Surprisingly, tanker type has relatively little influence, since tankers that

are more fuel efficient and therefore have lower carbon dioxide emissions have greater methane slippage in their exhaust. There are relatively few measurements of methane slippage, and I agree with others that it should be a priority to further explore slippage rates (Balcombe et al. 2022; Comer et al. 2024). The effect of tanker speed on emissions could also be further explored. In this analysis, I use average speeds for the world's LNG tanker fleet in recent years, but slower speeds lead to substantially greater efficiencies, reducing emissions of both carbon dioxide and methane (Rosselot et al. 2023). Nonetheless, emissions from tankers are a small part of the total for LNG.

The largest contributions to the greenhouse gas footprint for LNG exported from the United States are the upstream and midstream emissions from shale gas, particularly for methane. It should come as no surprise, therefore, that studies that assume lower methane emissions conclude that the overall LNG footprint is less than in my analysis. This is certainly the case for those assessments that rely on the GREET model and use the default methane emission factors from that model (NETL 2019; Gan et al. 2020). As noted above, the values used in the GREET model are based on unverified industry reporting to the US Environmental Protection Agency, and these estimates have been repeatedly found to be too low (see review by Howarth 2022). My methane emission factor is derived from the very latest data set from a large body of independent observations (Sherwin et al. 2014) and far better reflects the current state of the science.

Some LNG assessments compare methane and carbon dioxide using GWP₁₀₀ rather than GWP₂₀ (NETL 2019; Gan et al. 2020; Nie et al. 2020), although Rosselot et al. (2021) used GWP₂₀ as do many studies specifically focused on LNG tanker emissions (Pavlenko et al. 2020; Balcombe et al. 2021, 2022; Rosselot et al. 2023). Again, it should not be surprising that those analyses that rely on GWP₁₀₀ report lower total greenhouse gas emissions. While the 100-year time frame of GWP₁₀₀ is widely used in lifecycle assessments and greenhouse gas inventories, it understates the extent of global warming that is caused by methane, particularly on the time frame of the next several decades. The use of GWP₁₀₀ dates to the Kyoto Protocol in the 1990s, and was an arbitrary choice made at a time when few were paying much attention to the role of methane as an agent of global warming. As the Intergovernmental Panel on Climate Change stated in their AR5 synthesis report, "there is no scientific argument for selecting 100 years compared with other choices" (IPCC 2013). The latest IPCC AR6 synthesis reports that methane has contributed 0.5° C of the total global warming to date since the late 1800s, compared to 0.75° C for carbon dioxide (IPCC 2021). The rate of global warming over the next few decades is critical, with the rate of warming important in the context of potential tipping points in the climate system (Ritchie et al. 2023). Reducing methane emissions rapidly is increasingly viewed as critical to reaching climate targets (Collins et al. 2018; Nzotungicimpaye et al. 2023). In this context, many researchers call for using the 20-year time frame of GWP₂₀ instead of or in addition to GWP₁₀₀ (Ocko et al. 2017; Fesenfeld et al. 2018; Pavlenko et al. 2020; Balcombe et al. 2021, 2022). GWP₂₀ is the preferred approach in my analysis presented in this paper, as was the case for our earlier lifecycle assessment of blue hydrogen (Howarth & Jacobson 2021). Using GWP₂₀, LNG always has a larger greenhouse gas footprint than coal.

Increasingly, leaders on global climate policy are calling for a rapid move away from all fossil fuels, including natural gas and not just coal (Gaventa and Patukhova 2021; Figueres 2021). With an even greater greenhouse gas footprint than natural gas, ending the use of LNG should be a global

priority. I see no need for LNG as an interim energy source, and note that switching from coal to LNG requires massive infrastructure expenditures, for ships and liquefaction plants and the pipelines that supply them. A far better approach is to use financial resources to build a fossil-fuel-free future as rapidly as possible.

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Data availability

All data used in this paper are from publicly available sources that are identified in the manuscript.

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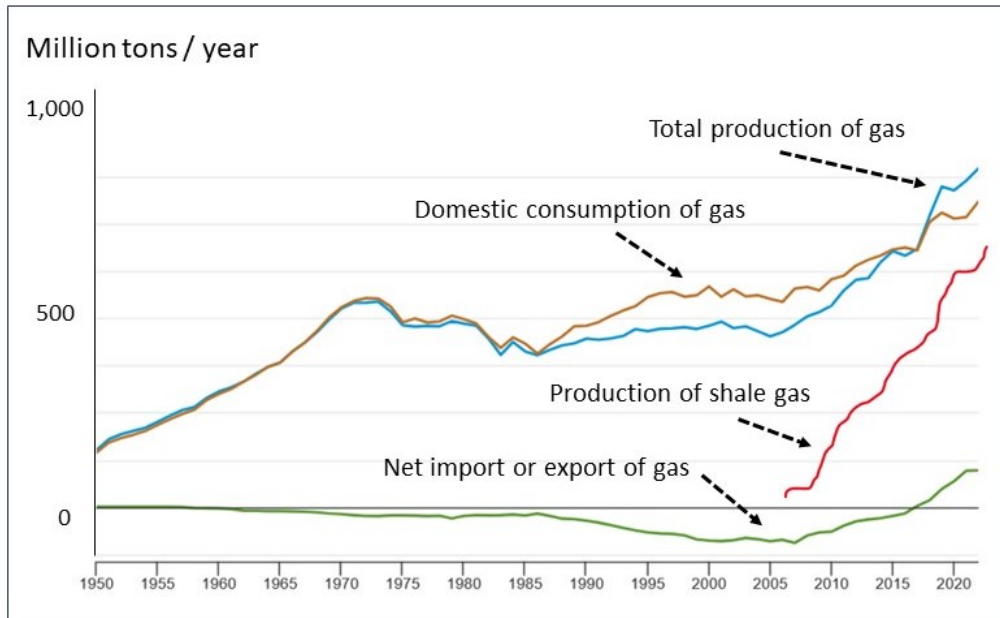


Figure 1. Trends in natural gas production in the United States from 1950 to 2022, showing total production of gas (conventional plus shale), production just of shale gas, domestic consumption, and the net import or export of gas. Almost all of the increase in natural gas production since 2005 has been shale gas. The United States was a net importer of natural gas from 1985 to 2015 but has been a net exporter since 2016.

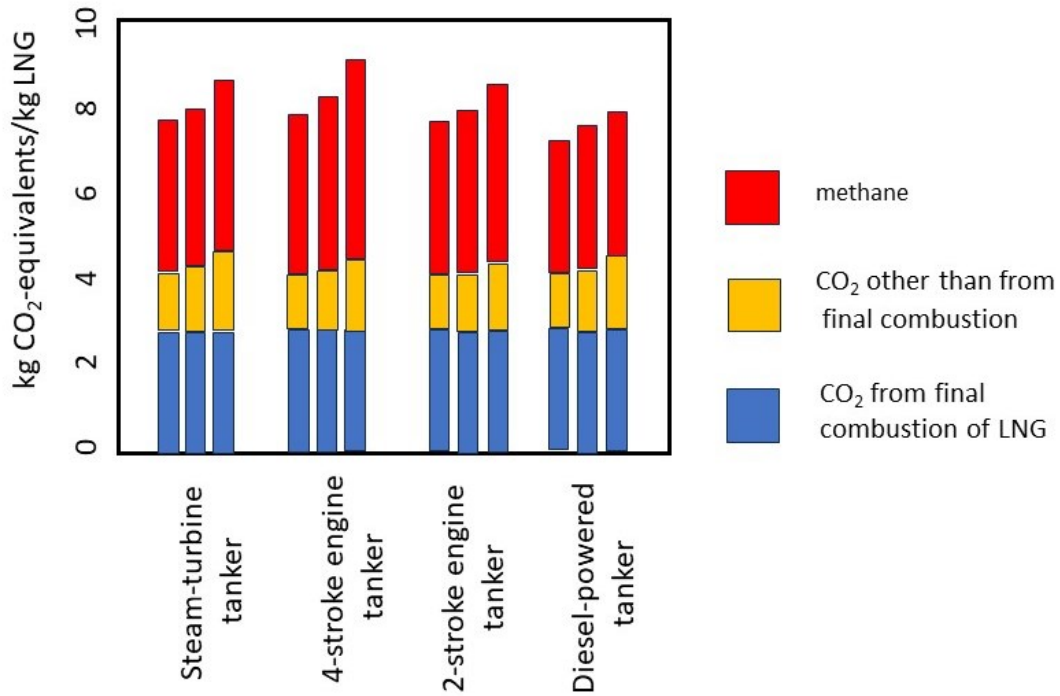


Figure 2. Full lifecycle greenhouse gas footprints for LNG expressed per mass of LNG burned by final consumer, comparing four scenarios where the LNG is transported by different types of tankers. For each type of tanker, scenarios are shown for shortest voyage times (bars to the left), average voyage times (center bars), and longest voyage times (bars to the right). Emissions of methane, the carbon dioxide emitted from the final combustion, and other carbon dioxide emissions are shown separately. Methane emissions are converted to carbon dioxide equivalents using GWP₂₀. See text.

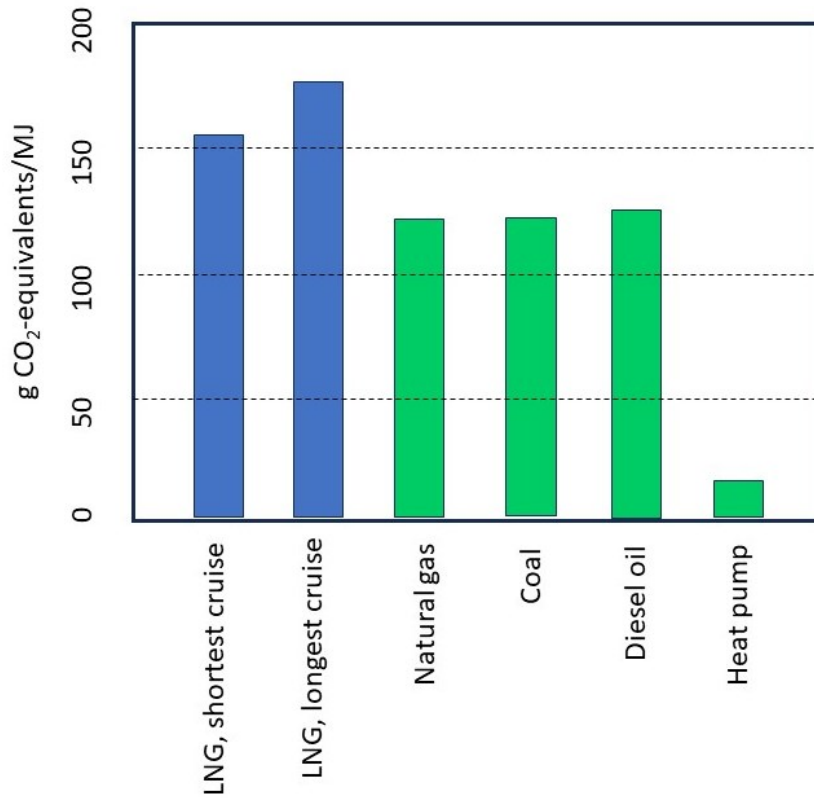


Figure 3. Full lifecycle greenhouse gas footprint for LNG for both short and long cruises compared to coal used domestically, diesel oil used domestically, natural gas used domestically, and electric-power ground source heat pump powered by the average European electric grid. The LNG values are the means for the three types of tankers that burn LNG for fuel. Methane emissions are converted to carbon dioxide equivalents using GWP₂₀. Note that values are expressed per unit of heat energy for each fuel for delivery to an electric generation plant. This does not include methane emissions from urban distribution systems that deliver to buildings for heat. Emissions for LNG and natural gas used domestically would both increase substantially for this use of gas. See text.

Table 1. Summary of some of the major input parameters used in LNG lifecycle assessment. See text for detailed derivations and discussion.

Stage	Equation	Parameter values	References
Upstream & midstream			
• Methane	Eq. 1	2.8% of production	Sherwin et al. (2024)
• CO ₂	Eq. 2	612 g CO ₂ /kg LNG	DEC (2021), Table A.1
Downstream methane	Eq. 3	0.0032 kg/kg LNG	Alvarez et al. (2018)
Liquefaction			
• Methane	Eq. 4	3.5 g CH ₄ /kg LNG	Balcombe et al. (2021)
• CO ₂	Eq. 5	270 + 57 + 18 g CO ₂ /kg LNG	Tamura et al. (2001); Okamura et al. (2007)
Tankers			
• Methane slip	Eq. 6	0%, 3.8%, or 6.4% of fuel burn	Pavlenko et al. (2020); Balcombe et al. (2022); Comer et al. (2024)
• Fuel consumption	Eq. 7, 8	108, 130, or 175 tons/day	Raza and Schoyen (2014); Bakkali & Ziomas (2019)
• Boil off	Eq. 9	0.00135 kg CH ₄ /kg per day	Hassan et al. (2009); Huan et al. (2018); Rosselot et al. (2023)
• Cargo volume	---	68,000 tons LNG	Raza and Schoyen (2014)
• Voyage times	---	21.4, 38, or 70 days round trip	Oxford Institute for Energy Studies (2018)

Table 2. Comparison of rate of unforced boil off and fuel needs to power different types of LNG tankers.

	Tons LNG per day
Unforced boil off, ambient temperature of 5° C	67.5 ^a
Unforced boil off, ambient temperature of 25° C	115 ^a
Boil off required for steam-powered tanker burning LNG	175
Boil off required for tanker powered by 4-stroke engines burning LNG	130
Boil off required for tanker powered by 2-stroke engines burning LNG	108

a) Assumes tanker gross cargo capacity of 67,500 tons. Unforced boil off is that which occurs due to heat leakage to LNG storage tanks. Tankers can increase boil off rate to meet fuel demand.

Table 3. Full lifecycle greenhouse gas emissions for LNG for 4 different scenarios for shipping by tanker, using world-average voyage times (38 day round-trip). Methane emissions are shown both as mass of methane and mass of CO₂ equivalents based on GWO₂₀. Values are per final mass of LNG consumed. Numbers in parentheses indicate the percent for each component of the total CO₂ equivalents.

	Carbon Dioxide	Methane		Total combined
	g CO ₂ /kg	g CH ₄ /kg	g CO ₂ -eq/kg	g CO ₂ -eq/kg
Steam-turbine tankers powered by LNG				
Upstream & midstream emissions	768 (9.9%)	36.1	2,982 (38%)	3,750 (48%)
Liquefaction	383 (4.9%)	3.9	320 (4.1%)	703 (9.0%)
Emissions from tanker	301 (3.9%)	0	0 (0%)	301 (3.9%)
Final transmission & distribution	0 (0%)	3.2	264 (3.4%)	264 (3.4%)
Combustion by final consumer	2,750 (35%)	0	0 (0%)	2,750 (35%)
Total	4,202 (54%)	43.2	3,566 (46%)	7,768
4-stroke engine tankers powered by LNG				
Upstream & midstream emissions	753 (9.4%)	35.4	2,920 (36%)	3,673 (46%)
Liquefaction	375 (4.7%)	3.8	314 (3.9%)	689 (8.6%)
Emissions from tanker	223 (2.8%)	5.2	429 (5.3%)	652 (8.1%)
Final transmission & distribution	0 (0%)	3.2	264 (3.3%)	264 (3.3%)
Combustion by final consumer	2,750 (34%)	0	0 (0%)	2,750 (34%)
Total	4,101 (51%)	47.6	3,927 (49%)	8,028
2-stroke engine tankers powered by LNG				
Upstream & midstream emissions	741 (9.6%)	34.9	2,876 (37%)	3,618 (47%)
Liquefaction	369 (4.8%)	3.7	309 (4.0%)	678 (8.8%)
Emissions from tanker	186 (2.4%)	2.6	212 (2.8%)	397 (5.2%)
Final transmission & distribution	0 (0%)	3.2	264 (3.4%)	264 (3.4%)
Combustion by final consumer	2,750 (36%)	0	0 (0%)	2,750 (36%)
Total	4,046 (52%)	44.4	3,661 (48%)	7,707
Diesel-powered tankers				
Upstream & midstream emissions	693 (9.4%)	32.6	2,689 (36%)	3,381 (46%)
Liquefaction	345 (4.7%)	3.5	289 (3.9%)	634 (8.6%)
Emissions from tanker	326 (4.4%)	0.2	15 (0.2%)	340 (4.6%)
Final transmission & distribution	0 (0%)	3.2	264 (3.6%)	264 (3.6%)
Combustion by final consumer	2,750 (37%)	0	0 (0%)	2,750 (37%)
Total	4,114 (56%)	39.5	3,256 (44%)	7,370

Table 4. Greenhouse gas emissions for LNG exported from the United States compared to those for diesel oil and coal produced domestically near the final site of consumption. LNG estimates are the averages for the three scenarios shown in Table 2 for tankers that are fueled by LNG, using world-average voyage times (38 days). Methane emissions are shown both as mass of methane and mass of carbon dioxide equivalents based on GWP₂₀. Values expressed per quantity of energy available from the fuel.

	Carbon Dioxide	Methane		Total combined
	g CO ₂ /MJ	g CH ₄ /MJ	g CO ₂ -eq/MJ	g CO ₂ -eq/MJ
Average for LNG				
Upstream & midstream emissions	15.5	0.73	60.1	75.6
Liquefaction	7.7	0.078	6.5	14.2
Emissions from tanker	4.9	0.053	4.4	9.3
Final transmission & distribution	0	0.066	5.4	5.4
Combustion by final consumer	55.0	0	0	55.0
Total	83.1	0.93	76.5	160
Diesel oil				
Upstream & transport emissions	15.8	0.40	33.0	48.8
Combustion by final consumer	75.0	---	---	75.0
Total	90.8	0.40	33.0	123.8
Coal used domestically				
Upstream & transport emissions	3.4	0.21	17.3	20.7
Combustion by final consumer	99.0	---	---	99.0
Total	102.4	0.21	17.3	119.7

On-line only supplemental materials:

Supplemental Table A. Methane emissions from both upstream and downstream associated with natural gas production in the Permian Basin for 8 campaigns as presented in Sherwin et al. (2024).

Campaign	upstream emissions (tons/hr) ^a	midstream emissions (tons/hr) ^b	total emissions (tons/hr)	production (tons/hr) ^c	percent emitted
Kairos NM Permian	48.8	78.9	127.7	1,952	6.5 %
CM Permian/2019	119	250.5	369.5	10,527	3.5 %
CM Permian/202	25.7	76.7	102.4	4,767	2.2 %
CM Permian/summer 2021	28.0	65.5	93.5	5,950	1.6 %
CM Permian/fall 2021	28.0	65.4	93.4	6,228	1.5 %
CM Permian F2021, boundary/2019	54.2	92.7	146.9	4,756	3.1 %
CM Permian F2021, Delaware/2019	30.7	50.6	81.3	3,613	2.3 %
CM Permian F2021, Midland/2019	23.8	42.4	66.2	1,143	5.8 %
Total			1,080.9	38,936	2.8 %^d

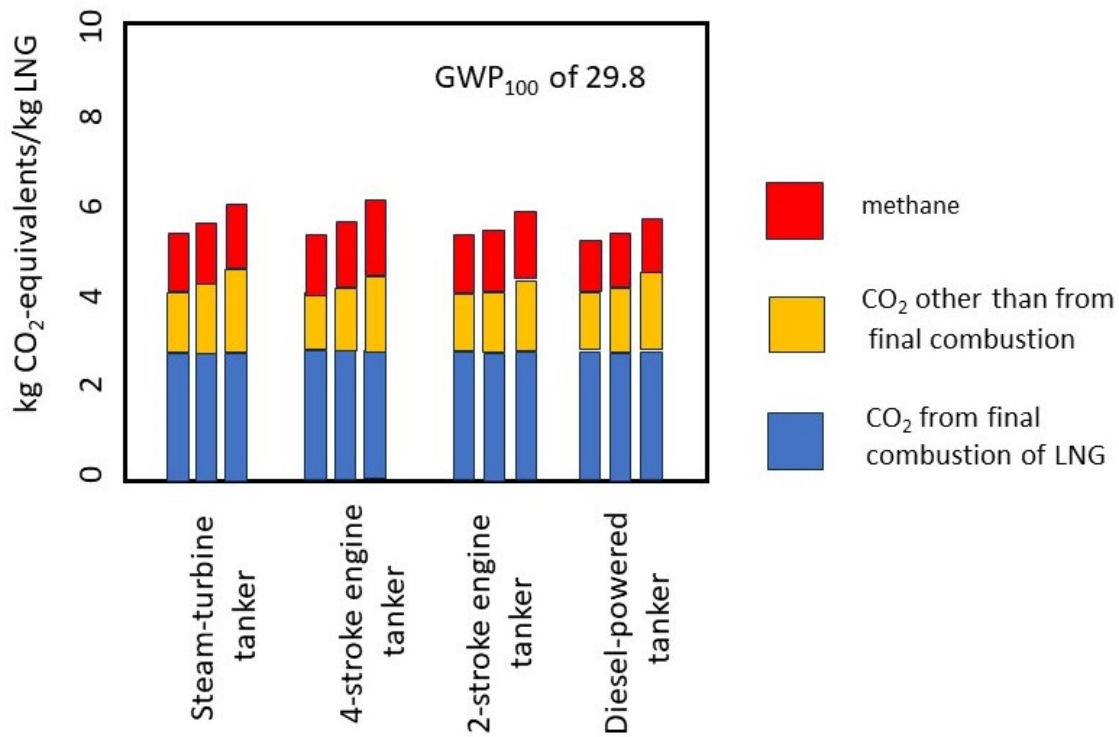
- Calculated from data in Table S10, Table S12, and Table S24 of supplemental material from Sherwin et al. (2024), with emissions weighted for natural gas vs oil considering energy basis.
- Calculated from data in Table S10 and Table S12 of supplemental material from Sherwin et al. (2024).
- From Table S10 of supplemental material from Sherwin et al. (2024)
- Percent of production emitted as methane weighted by the production occurring during each campaign.

Supplemental Table B. Full lifecycle greenhouse gas emissions for LNG for 4 different tanker-transport scenarios, using shortest voyages (21.4 days round-trip). Methane emissions are shown both as mass of methane and mass of CO₂ equivalents based on GWO₂₀. Values are per final mass of LNG consumed. Numbers in parentheses indicate the percent for each component of the total CO₂ equivalents.

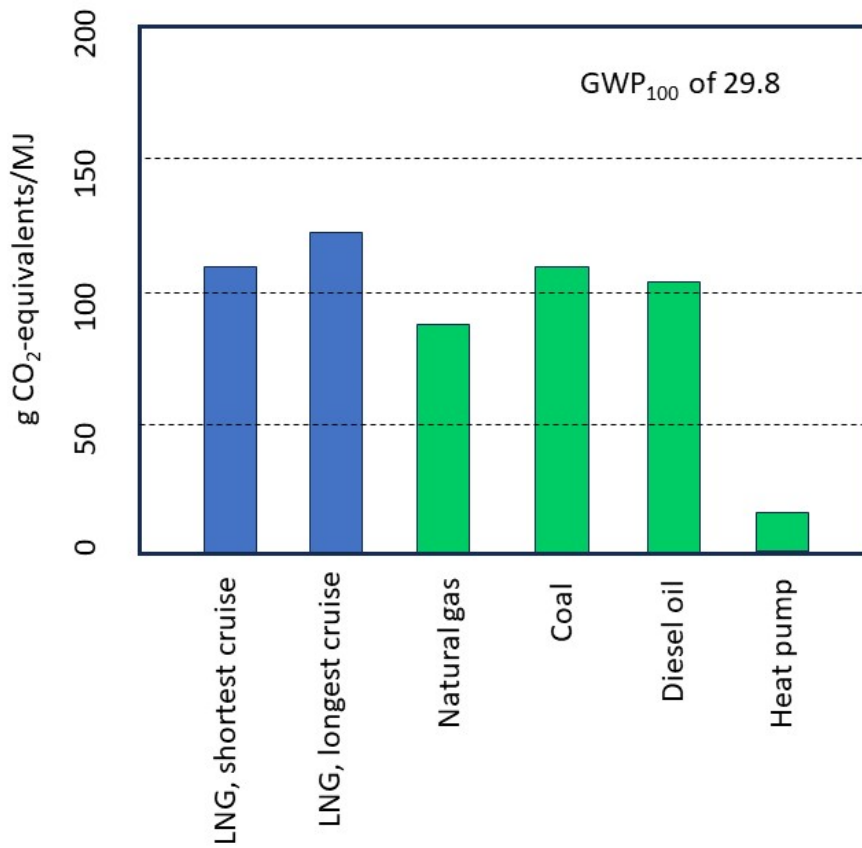
	Carbon Dioxide	Methane		Total combined
	g CO ₂ /kg	g CH ₄ /kg	g CO ₂ -eq/kg	g CO ₂ -eq/kg
Steam-turbine tankers powered by LNG				
Upstream & midstream emissions	735 (9.9%)	34.6	2,854 (38%)	3,589 (48%)
Liquefaction	366 (4.9%)	3.7	306 (4.1%)	673 (9.0%)
Emissions from tanker	169 (2.3%)	0	0 (0%)	169 (2.3%)
Final transmission & distribution	0 (0%)	3.2	264 (3.5%)	264 (3.5%)
Combustion by final consumer	2,750 (37%)	0	0 (0%)	2,750 (37%)
Total	4,021 (54%)	41.5	3,424 (46%)	7,445
4-stroke engine tankers powered by LNG				
Upstream & midstream emissions	727 (9.6%)	34.2	2,819 (37%)	3,545 (47%)
Liquefaction	362 (4.8%)	3.7	303 (4.0%)	665 (8.8%)
Emissions from tanker	126 (1.7%)	2.9	242 (3.2%)	367 (4.8%)
Final transmission & distribution	0 (0%)	3.2	264 (3.5%)	264 (3.5%)
Combustion by final consumer	2,750 (36%)	0	0 (0%)	2,750 (36%)
Total	3,964 (52%)	44.0	3,627 (48%)	7,591
2-stroke engine tankers powered by LNG				
Upstream & midstream emissions	720 (9.7%)	33.9	2,794 (38%)	3,514 (47%)
Liquefaction	359 (4.8%)	3.6	300 (4.0%)	659 (8.8%)
Emissions from tanker	104 (1.4%)	1.4	119 (1.6%)	224 (3.0%)
Final transmission & distribution	0 (0%)	3.2	264 (3.6%)	264 (3.6%)
Combustion by final consumer	2,750 (37%)	0	0 (0%)	2,750 (37%)
Total	3,933 (53%)	42.2	3,478 (47%)	7,411
Diesel-powered tankers				
Upstream & midstream emissions	693 (9.6%)	32.6	2,689 (37%)	3,381 (47%)
Liquefaction	345 (4.8%)	3.5	289 (4.0%)	634 (8.8%)
Emissions from tanker	183 (2.5%)	0.1	8.3 (0.1%)	192 (2.6%)
Final transmission & distribution	0 (0%)	3.2	264 (3.7%)	264 (3.7%)
Combustion by final consumer	2,750 (38%)	0	0 (0%)	2,750 (38%)
Total	3,971 (55%)	39.4	3,250 (45%)	7,221

Supplemental Table C. Full lifecycle greenhouse gas emissions for LNG for 4 different tanker-transport scenarios, using longest voyages (70 days round-trip). Methane emissions are shown both as mass of methane and mass of CO₂ equivalents based on GWO₂₀. Values are per final mass of LNG consumed. Numbers in parentheses indicate the percent for each component of the total CO₂ equivalents.

	Carbon Dioxide	Methane		Total combined
	g CO ₂ /kg	g CH ₄ /kg	g CO ₂ -eq/kg	g CO ₂ -eq/kg
Steam-turbine tankers powered by LNG				
Upstream & midstream emissions	833 (9.9%)	39.1	3,229 (38%)	4,061 (48%)
Liquefaction	415 (4.9%)	4.2	347 (4.1%)	761 (9.0%)
Emissions from tanker	554 (6.6%)	0	0 (0%)	554 (6.6%)
Final transmission & distribution	0 (0%)	3.2	264 (3.1%)	264 (3.1%)
Combustion by final consumer	2,750 (33%)	0	0 (0%)	2,750 (33%)
Total	4,551 (54%)	46.5	3,839 (46%)	8,390
4-stroke engine tankers powered by LNG				
Upstream & midstream emissions	803 (9.1%)	37.8	3,115 (35%)	3,918 (44%)
Liquefaction	400 (4.5%)	4.1	335 (3.8%)	735 (8.3%)
Emissions from tanker	412 (4.6%)	9.6	790 (8.9%)	1,202 (14%)
Final transmission & distribution	0 (0%)	3.2	264 (3.0%)	264 (3.0%)
Combustion by final consumer	2,750 (31%)	0	0 (0%)	2,750 (31%)
Total	4,364 (49%)	54.5	4,504 (51%)	8,869
2-stroke engine tankers powered by LNG				
Upstream & midstream emissions	782 (9.4%)	36.8	3,035 (37%)	3,817 (46%)
Liquefaction	390 (4.7%)	4.0	326 (3.9%)	716 (8.7%)
Emissions from tanker	342 (4.1%)	4.7	390 (4.7%)	732 (8.8%)
Final transmission & distribution	0 (0%)	3.2	264 (3.2%)	264 (3.2%)
Combustion by final consumer	2,750 (33%)	0	0 (0%)	2,750 (33%)
Total	4,264 (52%)	48.7	4,014 (48%)	8,277
Diesel-powered tankers				
Upstream & midstream emissions	693 (9.1%)	32.6	2,689 (35%)	3,381 (44%)
Liquefaction	345 (4.5%)	3.5	289 (3.8%)	634 (8.3%)
Emissions from tanker	600 (7.8%)	0.3	27 (0.4%)	627 (8.2%)
Final transmission & distribution	0 (0%)	3.2	264 (3.4%)	264 (3.4%)
Combustion by final consumer	2,750 (36%)	0	0 (0%)	2,750 (36%)
Total	4,388 (57%)	39.6	3,269 (43%)	7,656



Supplemental Figure A. Full lifecycle greenhouse gas footprints for LNG expressed per mass of LNG burned by final consumer, comparing four scenarios where the LNG is transported by different types of tankers. For each type of tanker, scenarios are shown for shortest voyage times (bars to the left), average voyage times (center bars), and longest voyage times (bars to the right). Emissions of methane, the carbon dioxide emitted from the final combustion, and other carbon dioxide emissions are shown separately. Methane emissions are converted to carbon dioxide equivalents using GWP₁₀₀. This figure is identical to Figure 2, except for converting methane emissions using GWP₁₀₀ rather than GWP₂₀.



Supplemental Figure B. Full lifecycle greenhouse gas footprint for LNG for both short and long cruises compared to coal used domestically, diesel oil used domestically, natural gas used domestically, and electric-power ground source heat pump powered by the average European electric grid. The LNG values are the means for the three types of tankers that burn LNG for fuel. Methane emissions are converted to carbon dioxide equivalents using GWP_{100} . This figure is identical to Figure 2, except for converting methane emissions using GWP_{100} rather than GWP_{20} . Note that values are expressed per unit of heat energy for each fuel for delivery to an electric generation plant. This does not include methane emissions from urban distribution systems that deliver to buildings for heat. Emissions for LNG and natural gas used domestically would both increase substantially for this use of gas.